

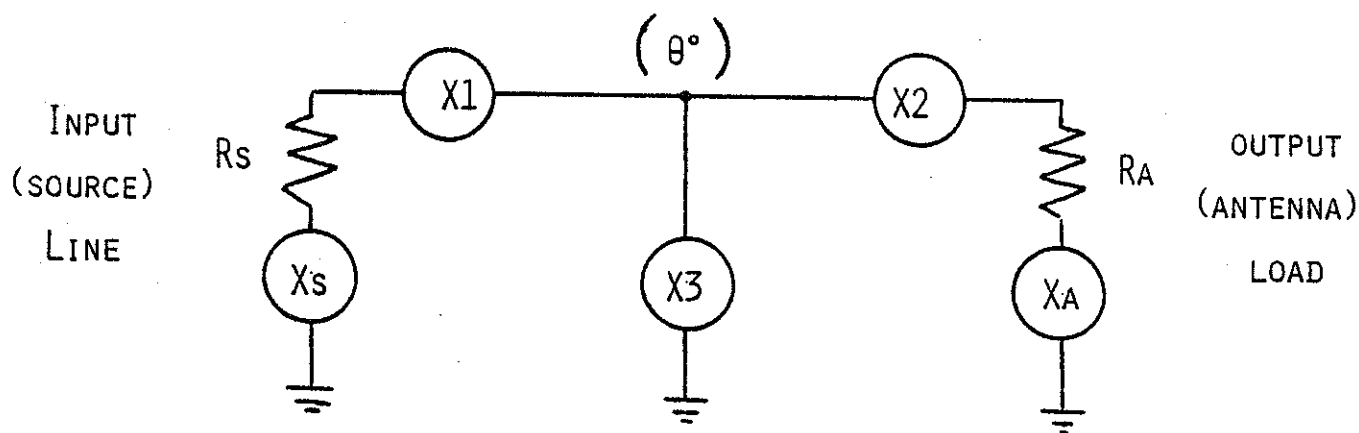
HOWARD & OTHER NETWORK INFORMATION:

GENERAL:

The attached information was prepared by George P. Howard, an authority on R.F. Network Designs to explain the differences between so called Howard and other types of networks.

DESIGN SHEET INFORMATION

(SYMBOL REFERENCES)



THE DESIGN SHEETS REFERENCE:

BRANCH 1 (THE INPUT ARM, X1) *

BRANCH 2 (THE OUTPUT ARM, X2) **

BRANCH 3 (THE SHUNT LEG, X3)

(RA): ANTENNA RESISTANCE (OR ANY LOAD RESISTANCE)

(XA): ANTENNA REACTANCE (OR ANY LOAD REACTANCE)

(Rs): TRANSMISSION LINE RESISTANCE (OR ANY DESIRED INPUT R_S)

(Xs): TRANSMISSION LINE REACTANCE (OR ANY DESIRED INPUT X_S)

(X1): INPUT ARM REACTANCE

(X2): OUTPUT ARM REACTANCE

(X3): SHUNT LEG REACTANCE

(Rp): THE EQUIVALENT PARALLEL RESISTANCE FOR A SERIES RESISTANCE AND REACTANCE

(THETA-T): THE NETWORK PHASE (DEGREES)

(TOTAL VOLT-AMPERE PRODUCT): THE SYSTEM'S STORED ENERGY

(Q): THE TOTAL SYSTEM STORED ENERGY; DIVIDED BY THE POWER,
IN WATTS.

THE Q OF THE ANTENNA IS X_A DIVIDED BY R_A ; THIS IS AN
INHERENT QUALITY AND CANNOT BE CHANGED WITHOUT MODIFY-
ING THE MANNER IN WHICH THE TOWER IS FED OR ITS BASIC
PHYSICAL DIMENSIONS AND CONSTRUCTION.

THE NETWORK Q IS THE TOTAL SYSTEM Q MINUS THE ANTENNA'S Q.

* FOR AN L NETWORK, THIS ARM "DISAPPEARS;" BECAUSE IT IN-
HERENTLY HAS A REACTANCE VALUE OF ZERO (WHEN R_A IS LESS
THAN R_s AND THE DESIRED X_s VALUE IS ZERO).

WHEN X_s IS NOT ZERO, THE NETWORK CAN STILL BE DESIGNED
TO PROVIDE AN X_1 ARM OF ZERO REACTANCE. THIS PROVISION
IS INCORPORATED IN THE DESIGN EQUATIONS.

** FOR AN RP NETWORK, THIS ARM "DISAPPEARS;" BECAUSE IT
INHERENTLY HAS A REACTANCE VALUE OF ZERO (WHEN THE LOAD
 R_p VALUE IS GREATER THAN THE DESIRED R_s VALUE).

IF THE LOAD R_p VALUE IS LESS THAN THE DESIRED R_s VALUE,
THE RP TYPE NETWORK CANNOT BE USED.

THE DESIGN EQUATIONS AUTOMATICALLY PROVIDE FOR X_s VALUES
OTHER THAN ZERO.

THE ANTENNA CURRENT, FOR BOTH TYPES, IS ALWAYS SHOWN IN
THE BRANCH 2 COLUMN.

HOWARD'S EQUATIONS

DESIGN EQUATIONS FOR SYSTEM NETWORKS

(FOR CALCULATION PURPOSES, TREAT NEGATIVE
RESISTANCES AS BEING POSITIVE)

1. FOR THE L TYPE NETWORK:

(THE DESIRED INPUT R_P VALUE MUST BE GREATER THAN THE
 R_A VALUE.)

IF IT IS NOT, USE THE R_P TYPE NETWORK AND ITS EQUATIONS.

L TYPE NETWORK EQUATIONS:

$$\text{LET } R_P = R_s + \frac{(X_s)^2}{R_s}$$

$$\theta = \left[\pm \text{ARC TAN} \left(\sqrt{\frac{R_P}{R_A} - 1} \right) + \text{ARC TAN} \left(\frac{X_s}{R_s} \right) \right]$$

$$X_3 = \frac{\sqrt{(R_A)(R_s)}}{\text{SIN } \theta}$$

$$X_2 = \frac{R_A}{\text{TAN } \theta} - (X_3) - (X_A)$$

2. FOR THE R_P TYPE NETWORK:

(THE LOAD R_P VALUE MUST BE GREATER THAN THE DESIRED
 R_s VALUE.)

IF IT IS NOT, USE THE L TYPE NETWORK AND ITS EQUATIONS.

RP TYPE NETWORK EQUATIONS:

$$\text{LET } R_P = R_A + \frac{(X_A)^2}{R_A}$$

$$X_1 = \left(\pm \sqrt{R_s (R_P - R_s)} \right) + (X_s)$$

$$\theta = - \left[\text{ARC TAN} \left(\frac{X_1 - X_s}{R_s} \right) + \text{ARC TAN} \left(\frac{X_A}{R_A} \right) \right]$$

$$X_3 = \frac{\sqrt{R_A R_s}}{\text{SIN } \theta}$$

3. FOR A TEE TYPE NETWORK:

$$X_1 = \frac{R_s}{\text{TAN } \theta} - (X_3)$$

$$X_2 = \frac{R_A}{\text{TAN } \theta} - (X_3) - (X_A)$$

$$X_3 = \frac{\sqrt{(R_A) (R_s)}}{\text{SIN } \theta}$$

FOR HOWARD EOR TYPE NETWORK:

(EQUAL AND OPPOSITE REACTANCES FOR INPUT ARM AND SHUNT LEG)

$$\theta = - 90^\circ \text{ FOR LAGGING PHASE}$$

$$\theta = + 90^\circ \text{ FOR LEADING PHASE}$$

$$\text{RESULTING INPUT } R_P = \frac{(X_1)^2}{R_A}$$

4. FOR A TEE TYPE NETWORK:

(WHERE THE INPUT IS A COMPLEX IMPEDANCE)

$$\theta_1 = \text{TAN}^{-1} \left(\frac{X_s}{R_s} \right)$$

$$\theta_3 = (\theta_T) + (\theta_1)$$

$$\angle A = (\pm 90^\circ) - (\theta_3)$$

USE -90° IF θ_T IS TO BE PLUS

USE $+90^\circ$ IF θ_T IS TO BE MINUS

$$X_4 = R_A \text{ TAN } \angle A$$

$$X_5 = R_s \text{ TAN } \angle A$$

THEN THE REQUIRED NETWORK ARMS ARE:

$$X_3 = \frac{\sqrt{(R_A)(R_s)}}{\text{SIN } \theta_3}$$

$$X_2 = (X_4) - (X_3) - (X_A)$$

$$X_1 = (X_5) - (X_3) + (X_s)$$

5. EQUATIONS FOR CALCULATING THE RESULTING INPUT IMPEDANCE OF A NETWORK:

(TREATING ALL NETWORKS AS TEE'S. WHERE X1 AND/OR X2 COULD BE ZERO; AND X3 COULD BE INFINITE)

$$\angle A = \text{TAN}^{-1} \left(\frac{(X_A) + (X_2) + (X_3)}{(R_A)} \right)$$

THEN:

$$R_s = \frac{(X_3)^2 (\text{Cos } A)^2}{(R_A)}$$

$$X_s = - \left(R_s \text{TAN } \angle A - (X_3) - (X_1) \right)$$

FOR THE NETWORK'S RESULTING PHASE-SHIFT:

$$\theta = (\pm 90^\circ) - (\angle A) - (\theta_1)$$

$$\text{WHERE: } \theta_1 = \text{TAN}^{-1} \left(\frac{X_s}{R_s} \right)$$

FOR THE ($\pm 90^\circ$):

USE $+90^\circ$ IF X3 IS PLUS

USE -90° IF X3 IS MINUS

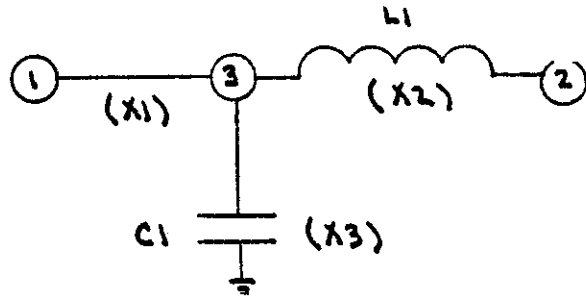
6. EQUATIONS FOR CALCULATING A TRANSMISSION LINE'S
"EQUIVALENT TEE NETWORK."

(FOR A LOSSLESS LINE WITH A PURE RESISTANCE CHARACTERISTIC
IMPEDANCE)

$$X1 = X2 = \left| Z_0 \tan \left(\frac{\theta}{2} \right) \right|$$

$$X3 = - \left| \frac{Z_0}{\sin \theta} \right|$$

EXAMPLES OF NETWORK COMPUTATIONS:



NETWORK: L Network

INPUT RA, XA, RS, DEGREES T 5, -75, 50, -71.565,

-71.565°
(DEGREES)

*****	X1	*****	X2	*****
RS + j XA (SOURCE)	-0.000		90.000	RA + j XA (LOAD)
50 j0				5 - j75
		X3		
		-16.667		

INPUT FREQ.(MHZ.), POWER(WATTS) T 0.62, 507,

	BRANCH 1 [INPUT]	BRANCH 3 [SHUNT]	BRANCH 2 [OUTPUT]
REACTANCE	-0.000	-16.667	90.000

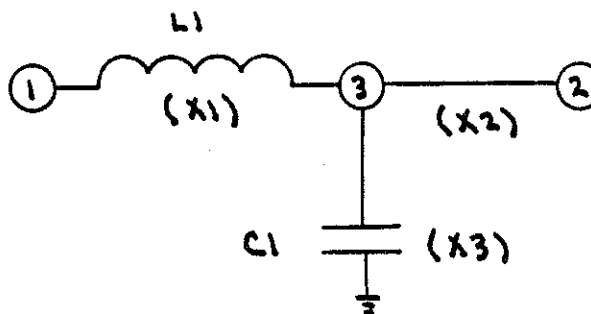
PFD OR MICRO-W *****	15402.085	23.103
RMS AMPS	3.184	9.553
MODULATED AMPS	3.900	11.700
RMS VOLTS	0.000	159.217
PEAK VOLTS	0.000	450.333
		2563.342

TOTAL VOLT-AMPERE PRODUCT 10647.002

Q 21.000

NETWORK SET-UP INFORMATION

	BRANCH 1	BRANCH 3	BRANCH 2
COMPONENTS :	None	C1	L1
MEASUREMENT1 (REF. POINT)	1 → 3	3 → Grnd	3 → 2
BR BRIDGE (DIAL X)	-0.00	-10.33	55.80
DELTA BRIDGE (DIAL X)	-0.00	-26.88	145.16



NETWORK: R_p Network

INPUT $R_A, X_A, R_B, \text{DEGREES } \theta$ 25, 100, 50, -145.904,

-145.904°
 (DEGREES)

*****	X1	*****	X2	*****
$R_S + j X_0$ (SOURCE)	136.930	*	-0.001	$R_A + j X_A$ (LOAD)
50 j0		*		25 j100
		*		
		X3		
		-63.069		

INPUT FREQ. (MHZ.), POWER (WATTS) ? .98, 3460,

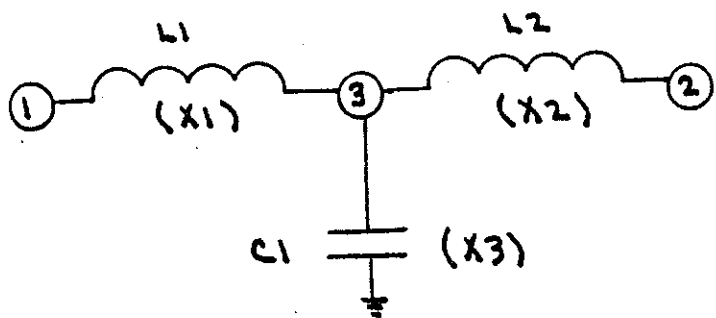
	BRANCH 1 [INPUT]	BRANCH 3 [SHUNT]	BRANCH 2 [OUTPUT]
EACTANCE	136.930	-63.069	-0.001
PFD OR MICRO-H.	22.238	2575.003	*****
RMS AMPS	8.319	19.227	11.764
MODULATED AMPS	10.188	23.548	14.408
RMS VOLTS	1139.072	1212.635	0.006
PEAK VOLTS	3221.782	3429.851	0.018

TOTAL VOLT-AMPERE PRODUCT : 32791.094

0 9.477

NETWORK SET-UP INFORMATION

	BRANCH 1	BRANCH 3	BRANCH 2
COMPONENTS :	L1	C1	None
MEASUREMENT: (REF. POINT)	1 → 3	3 → Grnd.	3 → 2
GR BRIDGE (DIAL X)	134.19	-61.81	-0.00
DELTA BRIDGE (DIAL X)	139.72	-64.36	-0.00



NETWORK: Tee Network

INPUT RA, XA, RS, DEGREES ? 210, -150, 50, -40,

	-60° (DEGREES)		
	X1	X2	
RS + J XA (SOURCE)	89.454	147.078	RA + J XA (LOAD)
50 j0			210 - j150
		X3	
		-118.322	

INPUT FREQ. (MHZ.), POWER (WATTS) ? 1.24, 2310,

	BRANCH 1 [INPUT]	BRANCH 3 [SHUNT]	BRANCH 2 [OUTPUT]
REACTANCE	89.454	-118.322	147.078
PFD OR MICRO-H	11.481	1084.762	18.878
RMS AMPS	6.797	5.887	3.317
MODULATED AMPS	8.325	7.210	4.062
RMS VOLTS	608.025	696.559	487.803
PEAK VOLTS	1719.753	1970.165	1379.714

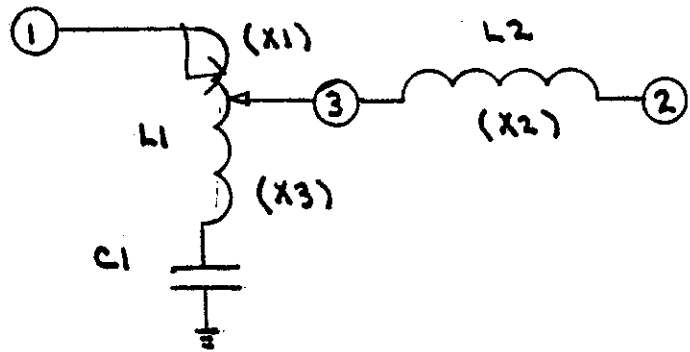
TOTAL VOLT-AMPERE PRODUCT 9851.276

Q 4.265

NETWORK SET-UP INFORMATION

	BRANCH 1	BRANCH 3	BRANCH 2
COMPONENTS :	L1	C1	L2
MEASUREMENT: (REF. POINT)	1 → 3	3 → Grnd	3 → 2
GR BRIDGE (DIAL X)	110.92	-146.72	182.38
DELTA BRIDGE (DIAL X)	72.14	-95.42	118.61

MULLANEY ENGINEERING, INC.



NETWORK: Howard EOR Network

INPUT RA, XA, RS, DEGREES ? 40, 60, 200, -90,

		-90° (DEGREES)		
*****	X1	*****	X2	*****
RS + J XA (SOURCE)	89.443	*	29.443	RA + J XA (LOAD)
		*		
		*		
200 j0		*		40 j60
		*		
		X3		
		-89.443		

INPUT FREQ.(MHZ.), POWER(WATTS) ? 1.5, 1200,

	BRANCH 1 [INPUT]	BRANCH 3 [SHUNT]	BRANCH 2 [OUTPUT]
REACTANCE	89.443	-89.443	29.443
PFD OR MICRO-H	9.490	1186.271	3.124
RMS AMPS	2.449	6.000	5.477
MODULATED AMPS	3.000	7.348	6.708
RMS VOLTS	219.089	536.656	161.264
PEAK VOLTS	619.677	1517.893	456.125

TOTAL VOLT-AMPERE PRODUCT 4639.876

0 3.867

NETWORK SET-UP INFORMATION

	BRANCH 1	BRANCH 3	BRANCH 2
COMPONENTS :	L1	L1/C1	L2
MEASUREMENT: (REF. POINT)	1 → 3	3 → Grnd	3 → 2
GR BRIDGE (DIAL X)	134.16	-134.16	44.16
DELTA BRIDGE (DIAL X)	59.63	-59.63	19.63